## Power \& Torque Imperial Standards

## Horsepower (HP)

Common unit of mechanical power, one HP is the rate of work required to raise 33,000 pounds one foot in one minute.


## One Imperial Horsepower Equals:

33,000 foot pounds per minute
36 inch pounds torque at 1750 RPM
.746 Kilowatts
1.014 Metric Horsepower (PS)
42.4 BTU per Minute

## Torque (T)

Torque is a twisting force. Torque causes rotation of a shaft, or it will set up a twist in a stationary shaft. It is generally expressed in foot pounds or in inch pounds. Torque is measured by the load or pull and by the distance of the pull from the center of a shaft.


## Calculation Examples

A cable wrapped around a 6" dia. drum must lift a 2500 pound weight. The drum rotates at 30 RPM.

## Metric

(SI) Standards

## Power (P)

The basic unit power measurement in the metric (SI) system is the Watt. 1000 Watts = 1 Kilowatt (kW)


## Torque (M)

Torque is a twisting force. Torque causes rotation of a shaft, or it will set up a

$$
M=\frac{9550 \bullet P}{R P M}
$$ twist in a stationary shaft. It is generally expressed in Newton-Meters.

## SI Symbols

$M=$ Torque $P=$ Power in Kilowatts
$\mathrm{N}=$ Newton Kfgm = Kilogram force meter
$\mathrm{m}=$ Meter N-m = Torque in Newton-Meters
$x=$ Multiplication Symbol

## Calculation Examples

A cable wrapped around a . 5 meter dia. drum must lift 5000 kilograms of weight. The drum rotates 50 RPM.

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\section*{MECHANICAL ENGINEERING FORMULAE}

To Calculate HP:
\(H P=\frac{F \times R \times R P M}{63025}\)
\(H P=\frac{2500 \times 3 \times 30}{63025}\)
\(H P=3.57\)

To Calculate T:
\[
\begin{aligned}
& T=F \times R \\
& T=2500 \times 3 \\
& T=7500 \text { inch pounds }
\end{aligned}
\]

To Calculate P:
Power in Kilowatts

To Calculate M:
Torque in Newton-Meters
\[
\begin{aligned}
& P=\frac{W \cdot g \cdot V}{1000} \\
& P=\frac{5000 \cdot 9.81 \cdot \frac{\pi .5 \cdot 50}{60}}{1000} \\
& P=64.2 \text { kilowatts }
\end{aligned}
\]
\[
\begin{aligned}
& M=\frac{9550 \bullet 64.2}{50} \\
& M=12262 \mathrm{Nm}
\end{aligned}
\]
\begin{tabular}{|c|c|c|c|c|}
\hline \multicolumn{6}{|c|}{ Conversion Factors } \\
\hline 1 Kilowatt \(=\) & \(1 \mathrm{~N}-\mathrm{m}=\) & \(1 \mathrm{kgfm}=\) & \(1 \mathrm{lb} \mathrm{ft}=\) & \(1 \mathrm{lb} \mathrm{in}=\) \\
\hline 1.341 & .10197 & \(9.807 \mathrm{~N}-\mathrm{m}\) & \(1.356 \mathrm{~N}-\mathrm{m}\) & \(.1129 \mathrm{~N}-\mathrm{m}\) \\
\hline Imperial & .73756 lb ft & 7.233 lb ft & .1883 kgfm & .0115 kgfm \\
\hline Horsepower & 8.8507 lb in & 86.796 lb in & 12 lb in & .083 lb ft \\
\hline
\end{tabular}
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\section*{LIFTING WITH MULTIPART EINE}

\[
\frac{\text { Total Load to be Pulled }}{\text { Single Line Pull in Pounds }}=\text { RATIO }
\]

Example:
To find the number of parts of line needed when weight of load and single line pull is established.

Sample Problem:
\(\frac{72480 \mathrm{lbs} . \quad \text { (load to be lifted) }}{8000 \mathrm{lbs} . \quad \text { (single line pull) }}=9.06\) RATIO
Refer to ratio 9.06 in table or number nearest to it, then check column under heading "Number of Parts of Line* ... 12 parts of line to be used for this load.

\section*{Example:}

To find single line pull needed when weight of load and number of parts of line are established.

Sample Problem:
68000 lbs . (load to be lifted)
6.60 (ratio of 8 part line) \(=1030 \mathrm{lbs}\) (single line pull)

10300 lbs . single line pull required to lift this load on 8 parts of line.

\section*{How To Calculate Line Parts}
\begin{tabular}{|c|c|c|}
\hline Number of Parts of Line & Ratio for Bronze Bushed Sheaves & Ratio for AntiFriction Bearing Sheaves \\
\hline 1 & . 96 & . 98 \\
\hline 2 & 1.87 & 1.94 \\
\hline 3 & 2.75 & 2.88 \\
\hline 4 & 3.59 & 3.81 \\
\hline 5 & 4.39 & 4.71 \\
\hline 6 & 5.16 & 5.60 \\
\hline 7 & 5.90 & 6.47 \\
\hline 8 & 6.60 & 7.32 \\
\hline 9 & 7.27 & 8.16 \\
\hline 10 & 7.91 & 8.98 \\
\hline 11 & 8.52 & 9.79 \\
\hline 12 & 9.11 & 10.6 \\
\hline 13 & 9.68 & 11.4 \\
\hline 14 & 10.2 & 12.1 \\
\hline 15 & 10.7 & 12.9 \\
\hline 16 & 11.2 & 13.6 \\
\hline 17 & 11.7 & 14.3 \\
\hline 18 & 12.2 & 15.0 \\
\hline 19 & 12.6 & 15.7 \\
\hline 20 & 13.0 & 16.4 \\
\hline 21 & 13.4 & 17.0 \\
\hline 22 & 13.8 & 17.7 \\
\hline 23 & 14.2 & 18.3 \\
\hline 24 & 14.5 & 18.9 \\
\hline
\end{tabular}

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\section*{Winch Sizing}

\section*{As a General Guide to Sizing the Right Winch for the Job, the Following Detail May Be of Help:}

\section*{Load}

Calculate the total weight of all the loaded railcars to be moved simultaneously. For example, if four loaded railcars, each weighing 85 tons are to be moved together, the total load will be four times 85 tons, for a combined weight of 340 tons.

\section*{Rolling Resistance Under Ideal Conditions}

Resistance to rolling is influenced by the wheel journals, type of lubrication used and the ambient temperature. Assuming the railcars are to be moved along a straight, level and well-maintained track, select the running line pull for the lowest anticipated temperature, using Table 1.

Example: If the lowest anticipated temperature is 32\&\#176F, the required running line pull from Table 1 will be \(15 \mathrm{lbs} / t o n\). Multiply the total weight of the railcars 340 tons by \(15 \mathrm{lbs} / t o n\) and the total running line pull becomes 5100 lbs .
\begin{tabular}{|c|c|c|c|c|}
\hline Temperature & More Than \(32^{\circ} \mathbf{F}\) & Less Than \(32^{\circ} \mathbf{F}\) & More Than \(0^{\circ} \mathbf{F}\) & Less Than \(-\mathbf{2 0}^{\circ} \mathbf{F}\) \\
\hline \begin{tabular}{c} 
Running Line Pull \\
(lbs/ton)
\end{tabular} & 12 & 15 & 20 & 25 \\
\hline
\end{tabular}

\section*{Track Gradient}

For each one percent gradient a rise of one foot for every 100 feet of track the running line pull must be increased by \(20 \mathrm{lbs} / t o n\).

Example: If the track has a \(1.5 \%\) grade, the additional running line pull is 20 , multiplied by 1.5 , or \(30 \mathrm{Ibs} / \mathrm{ton}\). The new
 is now calculated by multiplying \(45 \mathrm{lbs} / t o n\) by the 350 tons of railcars for a total of 15,300 lbs .

\section*{Track Curvature}

To overcome the effects of wheels binding against rails on curved sections of track, running line pull must be increased.

Track curvature is expressed in terms of radius or degree of curvature. When this information is not available, the chordal factor can be easily measured. Simply stretch a 50-foot tape along the inside of the curve and measure the distance ' \(A\) ' in Diagram 1.


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\section*{RAILCAR PULLING DETAIL}

Select the appropriate additional running line pull from Table 2 using either radius, degrees of curvature or chordal factor. (Interpolation for a measure of curvature is not shown.)
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{c} 
Radius \\
(ft)
\end{tabular} & \begin{tabular}{c} 
Degree of Curvature \\
(degree)
\end{tabular} & \begin{tabular}{c} 
Chordal Factor A \\
(in)
\end{tabular} & \begin{tabular}{c} 
Additional Running \\
Line Pull (lbs/ton)
\end{tabular} \\
\hline 1146 & 5 & 3.50 & 3.75 \\
\hline 573 & 10 & 6.50 & 7.50 \\
\hline 383 & 15 & 9.75 & 11.25 \\
\hline 288 & 20 & 13.00 & 15.00 \\
\hline 231 & 25 & 16.50 & 18.75 \\
\hline 193 & 30 & 20.00 & 22.50 \\
\hline 166 & 35 & 27.50 & 26.25 \\
\hline 146 & 40 & & 30.00 \\
\hline
\end{tabular}

Example: Chordal factor \(A\) was found to be 6.5 inches. The additional running line pull from Table 2 is 7.50 Ibs/ton. Now the running line pull has increased from \(45 \mathrm{lbs} / t o n\) to \(52.5 \mathrm{lbs} / t o n\). Again, multiplied by the 340 tons of railcars, the total running line pull is \(17,850 \mathrm{lbs}\).

\section*{Track Conditions}

If track conditions are substandard soft ballast, uneven or deteriorating ties or debris on the track additional running line pull will be needed. Since the condition of substandard track can vary considerably, Jeamar recommends that line pull be measured with a dynamometer.
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\section*{LOADS ON SHEAVES \& BLOGKS}

\section*{Determining The Stress On A Hook}

\section*{Multiply the Pull on the Lead Line By a Suitable Factor From the Following Table.} All Loads Shown Ignore Frictional Losses in the System.
\begin{tabular}{|c|c|}
\hline Angle & Factor \\
\hline \(0^{\circ}\) & 2.00 \\
\hline \(5^{\circ}\) & 1.998 \\
\hline \(10^{\circ}\) & 1.99 \\
\hline \(15^{\circ}\) & 1.98 \\
\hline \(20^{\circ}\) & 1.97 \\
\hline \(25^{\circ}\) & 1.95 \\
\hline \(30^{\circ}\) & 1.93 \\
\hline \(35^{\circ}\) & 1.90 \\
\hline \(40^{\circ}\) & 1.87 \\
\hline \(45^{\circ}\) & 1.84 \\
\hline \(50^{\circ}\) & 1.81 \\
\hline \(55^{\circ}\) & 1.77 \\
\hline \(60^{\circ}\) & 1.73 \\
\hline \(65^{\circ}\) & 1.69 \\
\hline \(70^{\circ}\) & 1.64 \\
\hline \(75^{\circ}\) & 1.58 \\
\hline \(80^{\circ}\) & 1.53 \\
\hline \(85^{\circ}\) & 1.47 \\
\hline \(90^{\circ}\) & 1.41 \\
\hline \(95^{\circ}\) & 1.35 \\
\hline \(100^{\circ}\) & 1.29 \\
\hline \(105^{\circ}\) & 1.22 \\
\hline \(110^{\circ}\) & 1.15 \\
\hline \(115^{\circ}\) & 1.07 \\
\hline \(120^{\circ}\) & 1.00 \\
\hline \(125^{\circ}\) & 0.92 \\
\hline \(130^{\circ}\) & 0.84 \\
\hline \(135^{\circ}\) & 0.76 \\
\hline \(140^{\circ}\) & 0.68 \\
\hline \(145^{\circ}\) & 0.60 \\
\hline \(150^{\circ}\) & 0.52 \\
\hline \(155^{\circ}\) & 0.43 \\
\hline \(160^{\circ}\) & 0.35 \\
\hline \(165^{\circ}\) & 0.26 \\
\hline \(170^{\circ}\) & 0.17 \\
\hline \(175^{\circ}\) & 0.08 \\
\hline \(180^{\circ}\) & 0.00 \\
\hline
\end{tabular}

The stress on a sheave or block varies with the degree of angle between the lead and load lines. When the two lines are parallel, 1000 pounds on the lead line results in a load of 2000 pounds on the hook. As the angle between the lines increases, the stress on the hook is reduced as illustrated below.


\section*{CALCULATING HEAD LOADS}

\section*{Note:}

Note: Since the rope is continuous, from the winch drum to the attachment point, the load is always 1 ton, no matter where measured. The head load is the number of line attachments at the head sheave \(x 1\) ton. All loads shown ignore frictional losses in the system.


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Minimum Distance from Drum to First Sheave or Load Connection - Feet


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\section*{Wire Rope Specifications}
\begin{tabular}{|c|c|c|}
\hline \multicolumn{3}{|c|}{ Preformed Galvanized Aircraft Cable 7x19 } \\
\hline \begin{tabular}{c} 
Size Diameter \\
(in)
\end{tabular} & \begin{tabular}{c} 
Weight per \\
100 ( lbs )
\end{tabular} & \begin{tabular}{c} 
Breaking \\
Strength (lbs)
\end{tabular} \\
\hline \(1 / 8^{\prime \prime}\) & 2.9 lbs. & \(2,000 \mathrm{lbs}\). \\
\hline \(3 / 16 "\) & 6.5 lbs. & \(4,200 \mathrm{lbs}\). \\
\hline \(1 / 4 "\) & 11.0 lbs. & \(7,000 \mathrm{lbs}\). \\
\hline \(5 / 16 "\) & 17.3 lbs. & \(9,800 \mathrm{lbs}\). \\
\hline \(3 / 8^{\prime \prime}\) & 24.3 lbs. & \(14,400 \mathrm{lbs}\). \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|}
\hline \multicolumn{3}{|c|}{ Steel I.W.R.C. 6x37 } \\
\hline \begin{tabular}{c} 
Size Diameter \\
(in)
\end{tabular} & \begin{tabular}{c} 
Weight per \\
100 ' (lbs)
\end{tabular} & \begin{tabular}{c} 
Breaking \\
Strength (lbs)
\end{tabular} \\
\hline \(7 / 16^{\prime \prime}\) & 33 lbs. & \(20,400 \mathrm{lbs}\). \\
\hline \(1 / 2^{\prime \prime}\) & 43 lbs. & \(26,600 \mathrm{lbs}\) \\
\hline \(9 / 16^{\prime \prime}\) & 54 lbs. & \(33,600 \mathrm{lbs}\). \\
\hline \(5 / 8^{\prime \prime}\) & 67 lbs. & \(41,200 \mathrm{lbs}\). \\
\hline \(3 / 4 "\) & 96 lbs. & \(58,800 \mathrm{lbs}\). \\
\hline \(7 / 8^{\prime \prime}\) & 131 lbs. & \(79,600 \mathrm{lbs}\). \\
\hline \(1 "\) & 170 lbs. & \(103,400 \mathrm{lbs}\). \\
\hline \(1-1 / 8^{\prime \prime}\) & 216 lbs. & \(130,000 \mathrm{lbs}\). \\
\hline \(1-1 / 4 "\) & 266 lbs. & \(159,800 \mathrm{lbs}\). \\
\hline \(1-3 / 8^{\prime \prime}\) & 322 lbs. & \(192,000 \mathrm{lbs}\). \\
\hline \(1-1 / 2^{\prime \prime}\) & 384 lbs. & \(228,000 \mathrm{lbs}\) \\
\hline \(1-5 / 8^{\prime \prime}\) & 450 lbs. & \(264,000 \mathrm{lbs}\). \\
\hline \(1-3 / 4 "\) & 522 lbs. & \(306,000 \mathrm{lbs}\). \\
\hline \(1-7 / 8^{\prime \prime}\) & 600 lbs. & \(384,000 \mathrm{lbs}\). \\
\hline \(2 "\) & 682 lbs. & \(396,000 \mathrm{lbs}\). \\
\hline
\end{tabular}

Grades - Slope \& Grade Resistance
\begin{tabular}{|c|c|c|}
\hline Grade (\% per 100 Horizontal ft) & Slope (Degrees \& Minutes per 100 Horizontal ft & Grade Resistance (lbs. Pull per Ton to Overcome Grade Resistance) \\
\hline 1 & 0-34 & 20 \\
\hline 2 & 1-9 & 40 \\
\hline 3 & 1-43 & 60 \\
\hline 4 & 2-17 & 80 \\
\hline 5 & 2-52 & 100 \\
\hline 6 & 3-26 & 120 \\
\hline 7 & 4-0 & 140 \\
\hline 8 & 4-34 & 160 \\
\hline 9 & 5-9 & 180 \\
\hline 10 & 5-43 & 199 \\
\hline 11 & 6-17 & 219 \\
\hline 12 & 6-51 & 238 \\
\hline 13 & 7-24 & 258 \\
\hline 14 & 7-58 & 277 \\
\hline 15 & 8-32 & 296 \\
\hline 16 & 9-39 & 315 \\
\hline 17 & 9-5 & 334 \\
\hline 18 & 10-12 & 353 \\
\hline 19 & 10-45 & 373 \\
\hline 20 & 11-19 & 392 \\
\hline 25 & 14-2 & 485 \\
\hline 30 & 15-17 & 575 \\
\hline 35 & 16-42 & 660 \\
\hline 40 & 21-48 & 743 \\
\hline 45 & 24-14 & 822 \\
\hline 50 & 26-34 & 895 \\
\hline 55 & 28-49 & 965 \\
\hline 60 & 30-58 & 1025 \\
\hline 65 & 33-1 & 1085 \\
\hline 70 & 34-59 & 1145 \\
\hline 75 & 36-52 & 1196 \\
\hline 80 & 38-40 & 1248 \\
\hline 85 & 40-22 & 1295 \\
\hline 90 & 41-59 & 1338 \\
\hline 95 & 43-32 & 1376 \\
\hline 100 & 45-0 & 1402 \\
\hline
\end{tabular}

\section*{Equivalent of Common Fractions of an Inch}

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